

The correction to pages 12 and 13 correct typographical errors.

The correction to page 14, line 3 is a correction of a clerical error. Support for this correction can be found in Table 1.

With respect to the correction to page 14, line 17; page 15, line 10; page 15, line 26; page 16, lines 19 and 20; page 19, Table 1; and page 20, Table 2 in the line marked "Tensile strength"; and in claim 7, lines 5 and 6 and the values of tensile strength in cN/decitex, applicants advise that the originally described values of tensile strengths are all defective because they were obtained by calculating in terms of tex numbering system. In the present specification, descriptions pertaining to size of yarns and properties of yarns are thoroughly given in terms of the decitex numbering system. Accordingly, conversions of the originally described cN/tex value into cN/decitex values ($1 \text{ cN/tex} = 0.1 \text{ cN/dtex}$) are not an introduction of new matter. For example, nylon 6.6 yarn having a tensile strength as high as 71 cN/decitex as originally described on page 14, line 17 cannot be imagined.

With respect to the corrections to page 14, line 18; page 15, lines 11 and 27; page 19, Table 1 and page 20, Table 2 in the line marked "Tensile work"; and in claim 7, line 7 and the values of tensile work at break in cN·cm/decitex, applicants advise that the tensile work at break is an integrated value from the initiation to a breakage point in a tensile stress strain curve divided by a yarn fineness and the divided integrated value is converted into cN·cm/decitex (see specification page 12, lines 24-32). The value is obtained by computation using a computer. The original described tensile work is faulty because the decimal point is erroneously positioned.

Schematically, this value is obtained by calculating the area of a triangle formed by the tensile strength value and value of elongation at break. Based on the tensile stress strain data obtained in Example 1, the tensile work at break is roughly calculated as follows:

$$\begin{aligned} &\text{Strength at break} \times \text{grip yarn length} \times \text{elongated} \\ &\text{value} \div 2 = 7.1 \times 20 \times 0.22 \div 2 = 15.6 \text{ cN}\cdot\text{cm}/\text{decitex} \end{aligned}$$

The correction to page 14, line 18 of 56 $\Delta n/1000$ to 0.056 is supported by Table 1 where values are given in $\Delta n \times 1000$. Applicants advise that in the science of fiber, birefringence (Δn) is frequently used as a parameter representing orientation of the polymer forming a fiber structure. For example, a commercially available nylon 66 fiber (yarn) has a birefringence of $40 - 70 \times 10^{-3}$. Table 1 shows $\Delta n \times 1000$, birefringence values are given in the present Examples. The description "56 $\Delta n/1000$ " is incorrect and is therefore corrected to read 0.056 (or 56×10^{-3}) in accordance with convention.

With respect to the correction to page 14, line 27, applicants advise that the product of total fineness of yarns in warp (or weft) multiplied by weave density in warp (or weft) is calculated for warp and weft directions of a fabric respectively. In Example 1, weave density for warp direction and weft direction are different (see Table 1); the weave fineness for warp is obtained by $156 \times 95 (= 14820)$, and that for weft is obtained by $156 \times 93 (14508)$. Weave densities for Examples and Comparative Examples are listed in Tables 1 and 2.

Finally, the corrections to page 15, lines 16 and 20 correct obvious omissions; support for the amendments to page 8, line 2 and page 17, line 13 can be found at page 16, lines 16 and 32; and support for the amendment to page 17, line 19 can be found in Comparative Example 1 in Table 2.

Entry of the amendments is therefore requested.

If there is any fee due in connection with the filing of this Statement, please charge the fee to our Deposit Account No. 06-0916.

Respectfully submitted,

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By: 

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